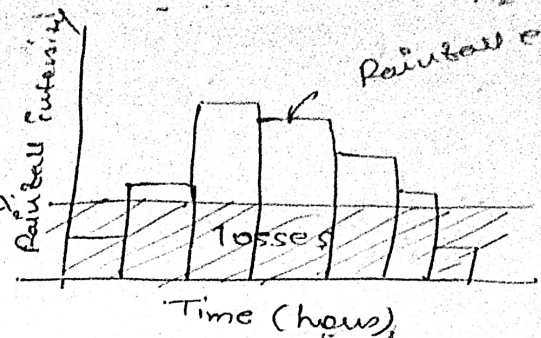


Hydrograph

Normal or irregularly missing data

$$P_x = \frac{H_x}{H-1} \left[\frac{P_1}{H_1} + \frac{P_2}{H_2} + \frac{P_3}{H_3} + \dots + \frac{P_n}{H_n} \right]$$

→ The initial loss and infiltration losses are subtracted from it. The resulting losses are subtracted from it. The resulting hydrograph is known as effective Rainfall Hydrograph.



→ expressed ERH is usually in cm/h plotted against time.

→ The area of ERH multiplied by the catchment area gives the total volume of direct runoff, which is the same as the area of DRH.

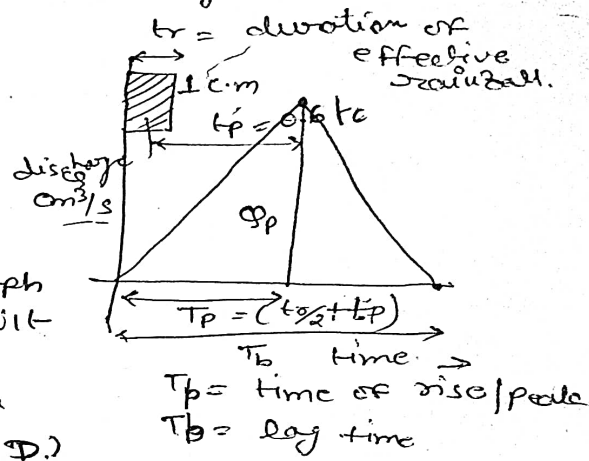
hydrograph of a storm.

$$\phi = \frac{\text{Rainfall} - \text{Runoff}}{\text{Total time}}$$

$$\phi = \frac{\text{Eff. Rainfall} - Q}{\text{Effective time}}$$

Unit Hydrograph

The problem of predicting the flood hydrograph resulting from a known storm in a catchment has received considerable attention.



A Unit Hydrograph is defined as the hydrograph of direct runoff resulting from one unit depth (1 cm) of rainfall excess occurring uniformly over the basin and a uniform rate for a specified duration (D-h) duration.

(basically triangular hydrograph method used in small watershed)
 SCS triangular Unit Hydrograph (Soil Conservation Service)

→ The net DRH, the estimated base flow is then added to obtain the total flood hydrograph.

$$[\text{Flood Hydrograph}] = [\text{DRH} + \text{base flow}]$$

$$Q_p = 2.08 \frac{A}{T_p} \text{ (m}^3\text{/s)}$$

$$t_p = 0.6 t_c$$

$$T_p = \left(\frac{t_r}{2} + t_p \right)$$

→ An empirical equation for the time interval N.

$$N = 0.83 A^{0.2}$$

A = drainage area in km²
N = in days

by log g...
 $T_b = 2.67 T_p$

Unit Hydrographs of different durations

Two methods are available for this purpose.

- Method of superposition
- The S-curve

- Unit Hydrograph = $\frac{\text{DRH}}{\text{ER}}$
- ER = $\frac{\text{derived } D - \text{hr } UH}{\text{used } D - \text{hr } UH}$
- triangular hydrograph
 $\frac{1}{2} Q \times T_b = \text{Volume}$
 $\frac{1}{2} \times Q \times T_b = \text{area} \times 1 \text{ cm}$
↑
Volume

Note: Transpiration measured by → Phytometer

① S-curve: - The average intensity of ER producing the s-curve is V_D cm/h and equilibrium discharge.

$$\Rightarrow Q_s = \frac{A}{D} \times 10^4 \text{ m}^3/\text{h}$$

A = area of catchment in km^2

D = duration in hours of ER of the unit hydrograph used in deriving the s-curve.

$$\Rightarrow Q_s = 2.778 \frac{A}{D} \times \text{m}^3/\text{s}$$

Use and limitation of unit hydrograph:-

- great use \rightarrow
- ① The development of flood hydrographs for extreme rainfall and hydraulic structure
 - ② extension of flood flow records based on rainfall records.
 - ③ development of flood forecasting and warning systems

Instantaneous Unit Hydrograph (IUH)

A finite unit hydrograph is indicated as the duration $D \rightarrow 0$. The limiting case of a unit hydrograph of zero duration is known as instantaneous unit hydrograph (IUH).

This IUH is a fictitious conceptual unit hydrograph which represents the surface runoff from the catchment due to an instantaneous precipitation of the rainfall excess volume of 1 cm.

Note ① The precipitation is collected and measured via a rain gauge. Term such as pluviometer, ombrometer and hyetometer.

② The average annual rainfall for the entire country is estimated as 118.8 cm (1183 mm)

$$\text{Coefficient of variation (Cv)} = \frac{100 \times \text{Standard deviation}}{\text{Mean}}$$

$\text{Standard deviation} = \sqrt{\frac{\sum (x_i - \bar{x})^2}{n}}$
 $\text{Mean} = \frac{\sum P_i}{n}$

③ The recurrence interval (also known as return period).

$$T = 1/p$$

If the probability of an event occurring is p ,

$$P_{r,n} = n C_r p^r q^{n-r} = \frac{n!}{(n-r)! r!} p^r q^{n-r}$$

① The probability of an event of exceedence probability p occurring 2 time in n successive year is,

$$P_{2,n} = \frac{n!}{(n-2)! 2!} p^2 q^{n-2}$$

② The probability of the event not occurring at all in n successive year is

$$P_{0,n} = q^n = (1-p)^n$$

Q) The probability of the event occurring at least once in a successive year

$$P_1 = 1 - q^n = 1 - (1 - P)^n$$

Imp Note

city) alcohol is found to be the most suitable chemical for use as an evaporation inhibitor. ① yield capacity
② quality

Two stage is importance in evaporation ① yield capacity
② quality

field capacity: field capacity is the maximum quantity of water that the soil can retain against the force of gravity.

Permanent wilting point: is the moisture content of a soil at which the moisture is no longer available in sufficient quantity to sustain the plants.

Infiltration Index :-

The defined average infiltration rate is called infiltration index and two group types of of Indices are in common

① φ-Index :- The average rainfall above which the rainfall volume is equal to the runoff volume. The φ-index is derived from the rainfall hyetograph with knowledge of the resulting runoff volume. The initial loss is also considered as infiltration.

Total rainfall $P = \sum_{i=h}^N I_i \cdot \Delta t$

Value of φ-index = then $P - \phi \cdot t_e = R_d$
 t_e = duration of rainfall excess.

$$\frac{P - R_d}{t_e} = \phi$$

Rational formula :-

$$Q = \frac{CIA}{3.6}$$

$I = \text{mm/h}$
 $A = \text{km}^2$
 $C = \text{constant}$

$C = \frac{A_1 C_1 + A_2 C_2 + A_3 C_3}{A_1 + A_2 + A_3}$

$\phi = \frac{\text{infiltration}}{\Delta t}$

② W-Index :- The initial losses are separated from the total abstractions and an average value of Infiltration rate, called W-index, is defined

$$W = \frac{P - R - I_a}{t_e}$$

P = total storm precipitation (C.U.)
 R = total storm runoff (C.U.)
 I_a = initial losses (C.U.)
 t_e = duration of rainfall process.

Imp Infiltration rate

Penball and runoff correlation CWC has found the following the estimation of φ index for flood producing storm.

$$R = \alpha I^{0.2}$$

$$\phi = \frac{I - R}{24}$$

α = coefficient depends upon soil type.
 P = runoff in cm from 24-h rainfall intensity
 I = intensity cm/h

The measurement of discharge in a stream - form an important branch of Hydrometry

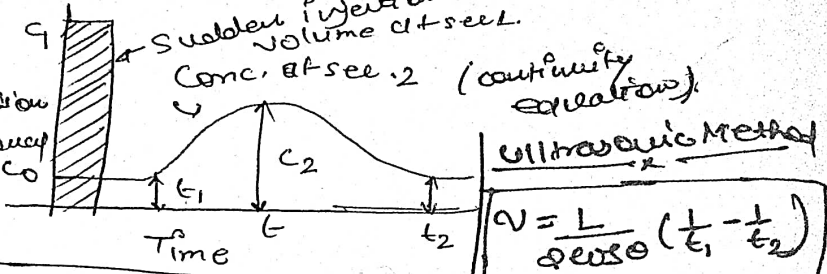
→ MEASUREMENT OF VELOCITY IS AN IMPORTANT ASPECT OF MANY DIRECT STREAM-FLOW MEASUREMENT TECHNIQUES. A MECHANICAL DEVICE, CALLED CURRENT METER,

⇒ Dilution Method :-

$$Q = Q_e \frac{(C_1 - C_2)}{(C_2 - C_0)}$$

C_1 = The tracer of concentration
 C_0 = The concentration Background value.

Chemical method :- (Steady flow) assumption



⇒ RUNOFF :- C_2 = constant value.

Interflow = prompt + delayed
 (direct) + indirect

Baseflow :- The delayed flow that reaches a stream essentially as groundwater flow is called base flow.

Baseflow = (delayed - interflow + Groundwater flow)

Runoff characteristics of stream

One to classify the stream in to three classes

- ① perennial ② intermittent ③ ephemeral.

① Perennial stream is one that,

↓ there is considerable amount of groundwater flow throughout the year. Even during the dry seasons,

② intermittent stream :- has limited contribution from the groundwater. During the wet season, there is contribution to the base flow to the stream flow. (baseflow + stream flow)

③ ephemeral stream :- is one that does not have any base-flow contribution.

① # Stream Density (S_d):- The ratio of the Number of streams N_s of all orders to the area of the basin (A) is known as stream density (S_d)

$$S_d = \frac{N_s}{A}$$

② Drainage Density (D_d):- The ratio of the total length of streams of all orders within a basin to its area.

$$D_d = \frac{\sum L}{A}$$

Note:- The term consumptive use is also used to denote the loss by evapotranspiration. Obviously dependent on the availability of water. Importance stage field capacity + wilting point

Different Catchment Shape Parameters:

(1) Form factor $\rightarrow \frac{\text{Catchment area}}{(\text{Catchment length})^2} = \frac{A}{L^2}$

(2) Slope factor $\rightarrow \frac{(\text{Catchment length})^2}{\text{Catchment area}} = \frac{L^2}{A}$

(3) Compactness coefficient $\rightarrow \frac{\text{Perimeter of the catchment}}{\text{Perimeter of the circle whose area is that of the basin}} = \frac{0.2821 P}{\sqrt{A}}$

(4) Circulatory ratio $\rightarrow \frac{\text{Catchment area}}{\text{Area of circle of catchment perimeter}} = \frac{12.57 A}{P^2}$

(5) Elongation ratio $\rightarrow \frac{\text{Diameter of circle}}{\text{catchment length}} = \frac{1.128 \sqrt{A}}{L}$

SCN-CN Method of Estimating Runoff Volume.

Basic theory \rightarrow SCN-CN Method is based on the water balance equation

$$P = I_a + F + Q$$

P = Total precipitation, I_a = initial abstraction

F = cumulative infiltration excluding I_a and Q

\Rightarrow direct surface runoff

100 represents a condition of zero potential abstraction
Catchment abstraction potential curve
retention, $CH=0$
precipitation infiltration abstraction
curve

$$Q = \frac{(P - 1.25S)^2}{P + (1 - 1.25)S} = \text{for } P > 1.25S$$

$$Q = 0 \text{ for } P \leq 1.25S$$

$$I_a = 1.25S$$

$$I_a = 0.25S$$

I_a = initial abstraction
↓
शुरुआत

Curve No. is now related to S as:

$$CN = \frac{25400}{S + 254}$$

$100 \geq CN \geq 0$
 S = potential maximum retention after runoff begins

CN depends upon

- (1) Soil type
- (2) Antecedent moisture condition
- (3) Land use/cover

Antecedent moisture conditions (AMC) (watershed wetness)
M.C present in the soil at the beginning of the rainfall runoff
three level of AMC are recognized by SCS as follows.

(1) AMC-I :- Soil wet but not wilting point, satisfactory cultivation has taken place (lowest runoff potential)

(2) AMC-II :- Average condition :-

(3) AMC-III :- Sufficient rainfall has occurred within immediate past 5 days. saturated soil conditions prevail.

\Rightarrow (highest runoff potential)

Impervious surface $c = 1.0$ and $CH = 0$ the relationship b/w CN and c are "inverse"

Sec-III Calculation for various conditions:

→ varying in the range 0.15 to 0.35

→ $Q = \frac{(P-0.15)^2}{P+0.95}$ for $P > 0.15$

valid for Black Soil under
Ame. of Type (II, and III)

→ $Q = \frac{(P-0.35)^2}{P+0.75}$ for $P > 0.35$ valid for Black Soil under
I, II, III types.

Compactness factor:

↳ $\frac{\text{Perimeter of watershed}}{\text{Circumference of circle}} = \frac{P}{2\pi R}$

Leaching requirement: "It is defined as the fraction of irrigation water passing out or drained out through the root zone, and expressed."

$LR = \frac{EC_w}{5EC_e - EC_w}$

where LR = minimum leaching requirement
EC_w = salinity of the applied irrigation water in dsm

EC_e = average soil salinity tolerated by crop, as measured on a soil. Saturated extract

$\frac{EC_w}{EC_e} = \frac{d_{dw}}{d_{iw}} = LR$

LR = important calculate

d_{dw} = depth of drainage water
the depth of irrigation water.

d_{iw} = depth of irrigation water.

EC_{iw} = Electrical conductivity of irrigation water.

EC_{dw} = Electrical conductivity of drainage water.

$D_i = \frac{1}{1-LR}$

$LR = \frac{d_{dw}}{d_{iw}} = \frac{d_{dw}}{d_{iw}} = \frac{EC_{iw}}{EC_e} = \frac{EC_{iw}}{2 \times EC_e}$

① Risk: $R = 1 - (1-P)^n = 1 - (1 - \frac{1}{T})^n$
P = probability = $\frac{1}{T}$

② Reliability: $R_e = 1 - R = (1 - \frac{1}{T})^n$

$S = K[xI^m + (1-x)Q^m]$

We know that $m=1$ putting value.
Now must use equation

(storage) $S = K[xI + (1-x)Q]$

Now evaluated

$Q = C_0 I_2 + C_1 I_1 + C_2 Q_1$ - ①

equation $x=0$, Now the storage.

is disc function of discharge is

Note ① Linear Storage and Linear Reservoir

$S = KQ$

① $C_0 = \frac{-Kx + 0.5 \Delta t}{K - Kx + 0.5 \Delta t}$

② $C_1 = \frac{Kx + 0.5 \Delta t}{K - Kx + 0.5 \Delta t}$

③ $Q = \frac{K - Kx - 0.5 \Delta t}{K - Kx + 0.5 \Delta t}$

Motor performance :

Rc

① Volumetric efficiency

$$\eta_v = \frac{D_m \times \omega_m}{\phi}$$

D_m = motor displacement
 ω_m = motor speed
 ϕ = flow rate.

② Torque efficiency / mechanical efficiency

$$\eta_T = \frac{T_L \times \omega_T}{D_m \times \Delta P}$$

T_L = Torque out
 ΔP = pressure drop across motor

③ overall efficiency

$$\eta_{oa} = \frac{P_{out} \text{ (actual power)}}{P_{in} \text{ (hydraulic power)}} = \frac{T_L \times \omega_m}{\phi \times \Delta P}$$

$$\eta_{oa} = \eta_v \times \eta_T = \frac{D_m \times \omega_m}{\phi} \times \frac{T_L}{D_m \times \Delta P} = \frac{\omega_m \times T_L}{\phi \times \Delta P}$$

④ accumulators :- storing energy in a hydraulic system

⑤ kinematic viscosity measured using many instrument by "saybolt universal viscometer"

⑥ The kingpin torque T required to turn the wheel under vertical load w.

Putting the value $\frac{I_0}{A} = \frac{b^2}{8}$ in equation ①

$$T = w f \sqrt{\frac{I_0}{A} + e^2}$$

f = effective friction coefficient
 I_0 = polar moment of inertia of tire
 e = kingpin offset
 A = tire print area
 w = vertical load

isotype permeability $\frac{b \times N_f}{\dots}$ No. of flow channels parallel to each other

$$T = w f \sqrt{\frac{b^2}{8} + e^2}$$

Dec - cm - Calculation for various conditions

Indicated work per revolution

$$W = \frac{P \cdot V_d}{N} \cdot \eta_m$$

$P = BPO$ (Brake power output)

$N = \text{engine speed rpm}$

$\eta_m = \text{mechanical efficiency}$

2) Air flow measurement that must pass through four stroke cycle engine.

$$Q (m^3/s) = \frac{\text{Displacement (litre)} \times \text{RPM} \times \text{Volumetric efficiency}}{60 \times 10^3}$$

3) Vibration is usually measured with Accelerometer

Effective temperature scale based on physiological response

$$\text{Transmissibility} = \frac{1}{\sqrt{1 + 4\zeta^2 \left(\frac{\omega}{\omega_n}\right)^2}}$$

$$\frac{1}{\sqrt{1 + 4\zeta^2 \left(\frac{\omega}{\omega_n}\right)^2}}$$

$\omega = \text{forcing ratio} = \frac{\omega}{\omega_n} = \frac{\text{seat excitation rate}}{\text{critical damping rate}}$

$\omega_n = \text{natural frequency}$

$\zeta = \text{undamped natural frequency of the seat}$

$$T = 2\pi \sqrt{\frac{I_0}{W}}$$

$I_0 = \text{Moment of inertia}$

$W = \text{weight of tractor}$

$R_0 = \text{distance b/w pivots. center of gravity of tractor.}$

4) Overturning condition in tire (moment)

$$W \cdot \frac{W}{R} \cos \gamma \cdot Z_{cg} - W_p A = 0$$

Moment arm = Tread width $\frac{a}{2} = \frac{a}{2}$

$$Z_{cg} = \sqrt{\frac{IAR}{W \cos \gamma}}$$

$A = \text{moment arm of C.G. (horizontal)}$
 $Z_{cg} = \text{height (vertical distance of C.G. from ground)}$

Volumetric efficiency :-

1) for cylinder

$$\eta_v = \frac{\text{actual volume of air taken into cylinder } m^3}{\text{ swept volume of air inside cylinder } m^3}$$

$$V_s = A \cdot L$$

$$\eta_v = \frac{V_{\text{actual}}}{V_s} = \frac{m}{P_a \times V_s \times \rho_{\text{air}} \times \eta_c}$$

1) diameter of actuator

$$D = \sqrt{\frac{4sT}{\pi P_a \eta_a}}$$

$D = \text{piston dia. mm}$

$s = \text{link to link steering}$

$T = \text{required torque}$

$s = \text{piston stroke mm}$

$P_a = \text{effective pressure at piston}$

$\eta_a = \text{actuator efficiency}$

$d = \text{piston rod dia.}$

$\eta_l = \text{linkage efficiency}$

2) displacement actuator

$$V = \frac{AT}{P_a \eta_l}$$